



**NAMIBIA UNIVERSITY  
OF SCIENCE AND TECHNOLOGY**

**FACULTY OF ENGINEERING AND SPATIAL SCIENCES**

**DEPARTMENT OF MECHANICAL, MINING AND PROCESS ENGINEERING**

<b>QUALIFICATION: BACHELOR OF ENGINEERING IN METALLURGY</b>	
<b>QUALIFICATION CODE: 08BMET</b>	<b>LEVEL: 8</b>
<b>COURSE CODE: MMY820S</b>	<b>COURSE NAME: MECHANICAL METALLURGY</b>
<b>SESSION: June 2023</b>	<b>PAPER: THEORY</b>
<b>DURATION: 3 HOURS</b>	<b>MARKS: 100</b>

<b>SECOND OPPORTUNITY QUESTION PAPER</b>	
<b>EXAMINER(S)</b>	<b>Prof. Sofya Mitropolskaya</b>
<b>MODERATOR:</b>	<b>Prof Josias Van der Merwe</b>

<b>INSTRUCTIONS</b>
<ol style="list-style-type: none"><li>1. Answer all questions.</li><li>2. Read all the questions carefully before answering.</li><li>3. Marks for each questions are indicated at the end of each question.</li><li>4. Please ensure that your writing is legible, neat and presentable.</li></ol>

**PERMISSIBLE MATERIALS**

1. Examination paper.

**THIS QUESTION PAPER CONSISTS OF 5 PAGES (Including this front page)**

**Question 1 [25 marks]**

(a) A low carbon mild steel at ASTM grain size of N1 ( $d=0,25$  mm) has revealed rather poor yield strength. Is it possible to triple the yield strength of the steel due to grain refinement to ASTM grain size of N8 ( $d=0,022$  mm)? With the aid of the Hall-Petch equation:

$$\sigma_y = \sigma_o + k\sqrt{\frac{1}{d}}$$

where  $\sigma_o$  and  $k$  are material constants,  $d$  is the grain size; estimate the yield strength growth of this steel as a result of such grain refinement. Note that for mild steel the lattice resistance stress  $\sigma_o$  is small and can be neglected.

[15]

Initial grain size (mm)	Grain size after refinement (mm)
0,25	0,022

(b) With the aid of Griffith's analysis of the critical stress:

$$\sigma_{\max} = \sigma_a (1 + 2a/b),$$

estimate the stress concentration  $\sigma_{\max}$  in the vicinity of an elongated non-metallic inclusion (Figure Q1). You may consider non-metallic inclusions as potential cracks. Assume the tensile stress  $\sigma_a$  is applied in vertical direction and equals 50 MPa.

[10]

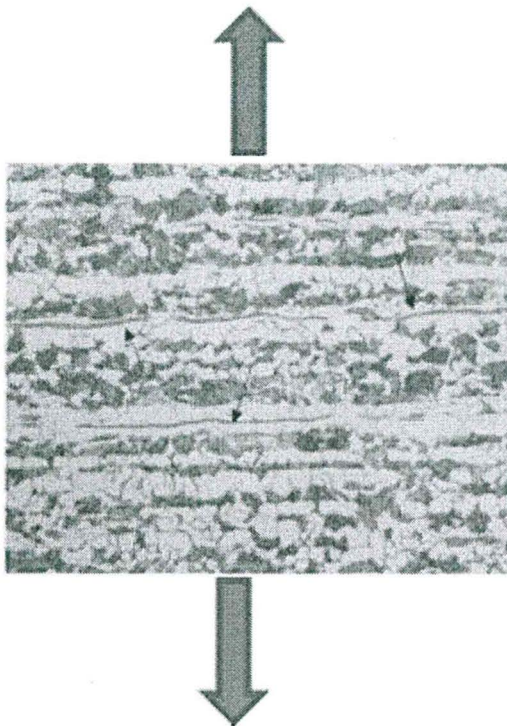
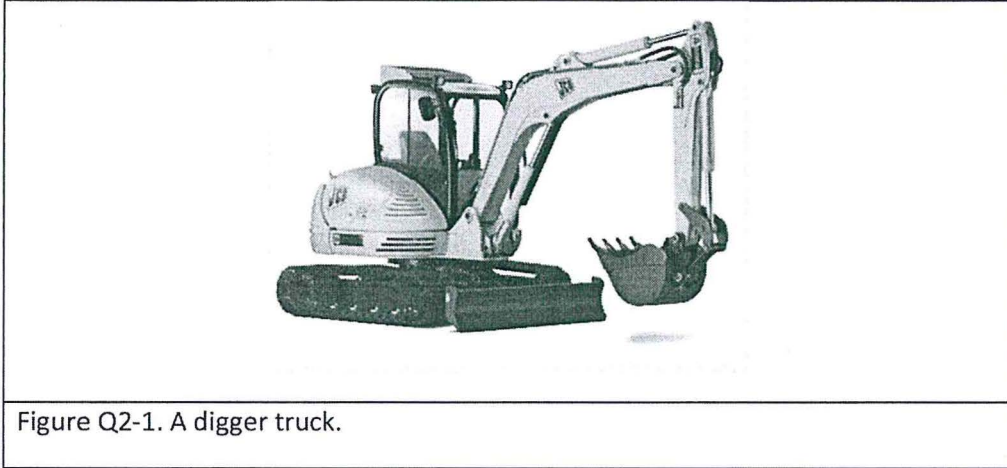


Figure Q1. Elongated non-metallic inclusions: length  $a=20$   $\mu\text{m}$ , width  $b=1$   $\mu\text{m}$

**Question 2 [25 marks.**

(a) You are asked to select a material for the teeth of a digger truck (Figure Q2-1). To do so you need to prioritize the materials properties that matter. List the key material properties required for the teeth of a digger truck. [6]



(b) Figure Q2-2 features stress-strain diagrams for a medium carbon steel, a mild steel, an Al alloy, brass (a solid solution of zinc in copper), and copper.

- (i) Roughly estimate the yield strength (or if appropriate a 0.2% proof stress) of each alloy. [3]
- (ii) Roughly indicate the tensile strength of each alloy. Fill in the table provided. [3]
- (iii) Which technological methods are available for strength increase of a mild steel by grain refinement? [3]

	Medium carbon steel	Mild steel	Al alloy	Annealed brass	Drawn brass	Annealed copper
Yield strength, MPa						
Tensile strength, MPa						

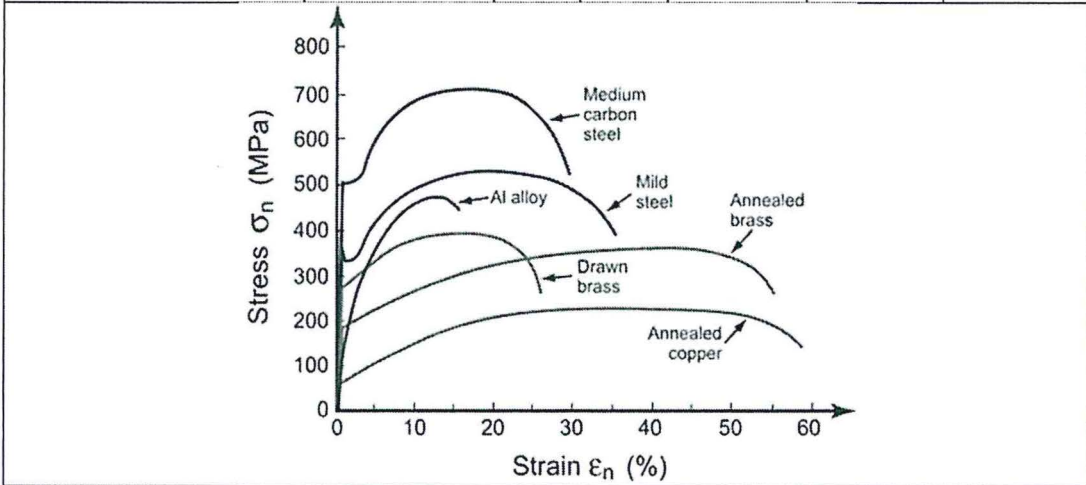


Figure Q2-2. Stress-strain curves for a selection of engineering alloys.

- (c) The critical strength  $\sigma_c$  of zinc is as low as 2 MPa. Ultrasonic non-destructive inspection of a zinc plate has revealed a crack 1 mm long ( $2a = 1$  mm). Is it safe to operate such a plate under Griffith's plain stress? Estimate with the aid of Griffith's criterion:

$$\sigma_c = \sqrt{\frac{2E\gamma_s}{\pi a}}$$

where  $\sigma_c$  is the critical stress required for propagation of the brittle crack (Pa);

$\gamma_s$  is the energy of the new surface area per unit of area;

E is Young's modulus (Pa)

a is a half-length of a critical crack that will propagate spontaneously;  $\pi = 3,14$ .

Make use of the following parameters:

	$\sigma_c$ , MPa	$\gamma_s$ , J/m <sup>2</sup>	E, GPa
Zinc	2	0,8	35

[10]

### Question 3 [25 marks]

- (a) Some bicycle forks are subjected to fatigue loading. Figure Q3-1 features the S–N diagram for the low-alloy steel used.

- (i) What is the 'fatigue limit' of the material? Estimate the fatigue limit of this steel. [5]
- (ii) The loading cycle due to road roughness is assumed to have a stress amplitude  $\sigma_a$  of 1200 MPa. How many loading cycles will the forks withstand before failing [5]
- (iii) Components that are susceptible to fatigue are sometimes surface treated by 'shot peening'. Explain how the process works, and why it is beneficial to fatigue life. [5]

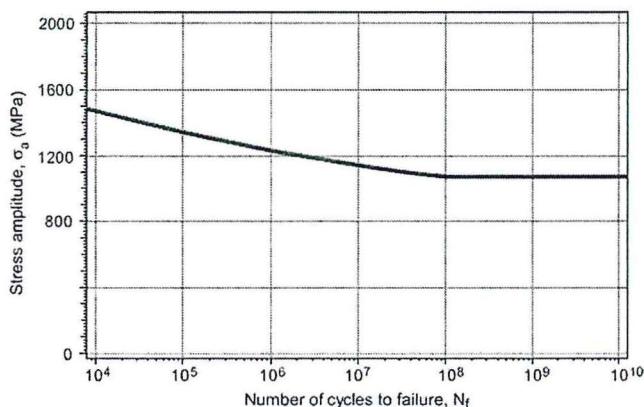


Figure Q3-1. Fatigue behaviour of low-alloy steel.

- (b) Why does a low carbon mild steel become brittle in the heat-affected zone next to a weld joint? No mechanical stress was applied [5]
- (c) Engineering creep is observed when a metal part is subjected to constant load at elevated temperature. Is creep a typical problem in Africa? [5]

**Question 4 [25 marks]**

A premature failure of lifting-fork arm was reported to a lift-truck manufacture (Figure Q4-1). The failure occurred in the elbow region of the lifting-fork arm. Lifting-fork arms are normally made of alloyed steel EN25 (0,3 %C; 2,5 %Ni; 0,6 % Cr; and 0,5 % Mo) by forging followed by heat treatment (quenching from 850 °C into oil and tempering under 600 °C for 1 hour). This treatment produces tempered martensite with the hardness of HV600. A group of failure investigators identified the chemical composition of the failed fork arm (see Table Q4) and examined the fracture surface (see Figure Q4-2). The microstructural examination of the failed arm revealed coarse bainite (Figure Q4-3). Vickers hardness measurement revealed the hardness of HV440.

- (i) Which metallurgical defect is responsible for the failure? [9]
- (ii) Briefly comment on the most likely failure mode. [8]
- (iii) What should be done to prevent the same failure in future? [8]

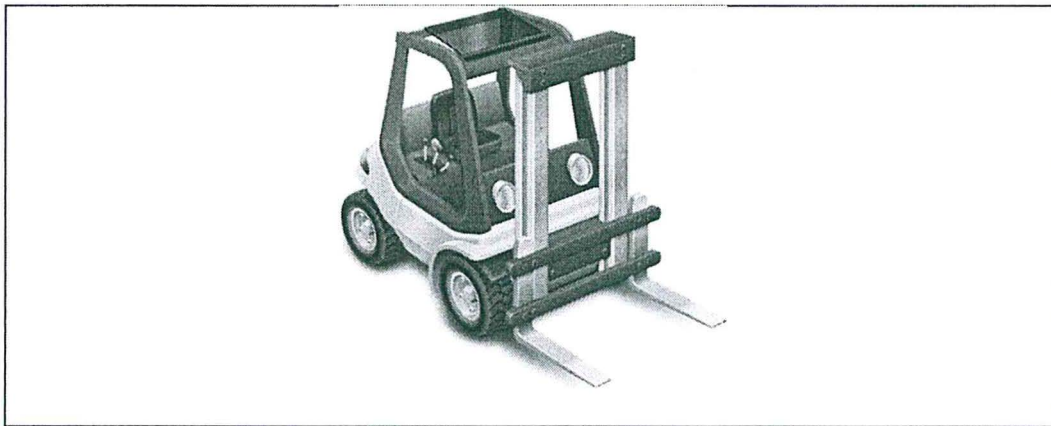


Figure 4-1. A lift truck with lifting-fork arms.

Table Q4. Lifting-fork arm steel chemical composition, as revealed.

C	Si	Mn	Ni	Cr	Mo	S	P
0.30	0.25	0.60	2.50	0.60	0.50	0.025	0.025



Figure 4-2. The fracture surface observed. X100

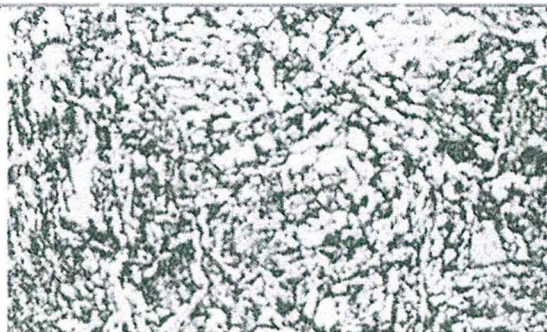


Figure 4-3. Microstructure of the coarse bainite. Metallographic microscopy, X400.

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